Development of Low-Power Wireless Sensor Network of Conductivity Probes for Detection of Corrosive Fluids Inside Pressure Vessels and Piping

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# **Project Objectives**

1. Develop the electronic components necessary to power and connect an array of conductivity sensors via a low-power, wireless sensor network (WSN).

2. Design, prototype and test conductivity probes compatible with standard access fittings and integrated into corrosion coupon holders.

3. Engage a significant number of students in the development of technology that is relevant to the pipeline industry and introduce them to the roles and responsibilities of producers and regulators (e.g. PHMSA) in the oil and gas sector.

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#### I. Electrical Conductivity





II. Electrical conductivity of fluids (electrolyte)





III. Double layer, polarization, equilibrium potential

(-)Electrode  $(\mathbf{f})$  $(\mathbf{f})$ Ð (+) $( \mathbf{f} )$  $(\mathbf{f})$ (-)Distance from Electrode Potential Potential Drop Φ **Diffuse** Layer OHP

Double layer will exist at any conductor/electrolyte interface

Double layer is very small (on the order of nanometers)

Behavior can be effectively modeled with a capacitor/resistor:



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#### Key takeaways:

- Corrosion reactions are electrochemical and require electrical current to flow between two sites.
- No current flow = no corrosion, No electrolyte = no current flow = no corrosion
- The ability to detect the presence of an electrolyte can give a warning for corrosion
- Potential (voltage) gradient over the double-layer is not instantaneous, but may approach a steady state value over time.
- Potential (voltage) gradient due to resistance (AKA Ohmic) is instantaneous.
- When we study corrosion we are primarily interested in the double-layer potential gradient.
- When we make conductivity/resistivity measurements we are interested only in the Ohmic potential gradient.



## IV. Conductivity / Resistivity Measurements

#### Steady State:

- Wenner (4-pin)
- Dissimilar metal comparison (galvanic cell)

#### Transient:

- Current Interrupt (Instant Off)
- AC (alternating current), Electrochemical Impedance Spectroscopy (EIS)

#### **Results:**

- Quantitative (e.g. 10  $\mu S/cm$ ) .... 1 Siemen (S) = 1  $\Omega^{-1}$
- Semi-Quantitative (e.g. low, medium, high)
- Binary (e.g. conductive or not conductive)



#### Measuring electrolyte resistivity:





#### V. How do we access the inside of an operational pipeline?









#### V. Wireless Sensor Networks

#### Pros:

- Each node can be independently powered by energy harvesting devise
- Lack of wired power/coms
- Resilient network if arranged in a mesh (multiple communication pathways)
- Relatively low cost

#### Cons:

- Limited computational power and precision of nodal microprocessor
- Relatively low temporal resolution
- Potentially slow data propagation rates
- May require (expensive) certification to operate in potentially explosive atmosphere (e.g. ATEX, IECEx, NFPA 70, CSA C22.1, etc.)



# **Project Team**

Dr. Matthew Cullin, UAA, ME (PI)

- Dr. Raghu Srinivasan, UAA, ME (co-PI)
- Dr. Todd Petersen, UAA, EE (co-PI)

Dr. John Lund, Western Washington University, EE (co-I)

1 Graduate student (M.S.) 12 Undergraduate ME and EE students

Industry Working Group (BPAK, Hilcorp, LLC / Harvest AK, LLC)





I. Probe analysis and design

A. Conductivity sensing element (electrodes) B. Access-fitting-compatible probe body C. Test vessel

II. Conductivity measurement technique development

III. Energy harvesting element design and analysis

IV. Wireless Sensor Network (WSN) integration and testing



#### **Design Requirements**

Support 2- and 4- electrode measurement techniques

1000 psig operating pressure

200°F operating temperature

Ability to be integrated into corrosion coupon holders (hydraulic access fitting)

Support low-power operations

Resist or support detection of electrode fouling



#### Approach

**COMSOL** Multiphysics modelling

Explore electrode size, shape, and spacing options in terms of impact on:

- Probe sensitivity
- Pipeline operations (e.g. pigging, coupon holder integration)
  - Power consumption
    - Electrode fouling





#### **Results** Potential distribution across linear configuration flush electrodes







**Results** Sensitivity analysis 100 mA



#### Design

3 mm diameters electrodes

linear configuration

5 mm center-to-center spacing

Electrode material: nickel alloy (e.g. C-276)

Electrode seals: glass





# I-B: Analysis/design of probe body

#### **Design Requirements**

Ability to integrate corrosion coupon holder

1000 psig operating pressure

200°F operating temperature

Corrosion resistant alloy

Installation in 2-inch hydraulic access fitting

Resist drag forces for 100% oil @ 15 ft/s



# I-B: Analysis/design of probe body

**Design** Detachable (optional) corrosion coupon holder





# I-B: Analysis/design of probe body

#### Design

FEA stress analysis

316L body

Coupons perpendicular to flow

FOS = 3.8







316L body material

Primary glass seals (electrodes) and secondary glass seals (wire bulkhead)

Rohrback Cosasco Inc. confirmed the ability to manufacture and incorporate into their adjustable positioning

Cost: \$2000 (prototype), \$700 for each additional unit

Full prototype not pursued due to limitations of integrating WSN electronics in explosive atmospheres.

Functional prototype of sensing element constructed instead



# I-C: Analysis/design of test vessel

Original intent: to test full prototype of probe

Modified intent: pressure vessel design exercise for ME undergraduate students

#### **Design Requirements**

1000 psig operating pressure

200°F operating temperature

2-inch hydraulic access fitting

Working fluid: water



# I-C: Analysis/design of test vessel

**Design** Thermal analysis (FEA)









# I-C: Analysis/design of test vessel

#### **Design Summary**

Design-by-rule based (ASME B31.4)

API 5L Grade A

NPS 6 Sch. 40 pipe body and end cap

Standard access fitting and threadolets

Class 600 flange

750W (120 VAC) heater, 1.25-inch NPTM connection

Designed under the supervision of piping engineer from BPXA



#### 4-electrode circuit diagram

- When digital out is high, voltage divider (R1, R2) determines the magnitude of a constant current source acting between the outer electrodes via LM324 buffer op amp.
- One differential instrumentation op amp (AD623) reads the voltage between the inner electrodes
- A second differential instrumentation op amp (AD623) reads the voltage over a shunt resistor, to verify the current.





#### Method #1: Wenner (steady state)

- Apply fixed current between outer electrodes
- Monitor voltage across inner electrodes and wait for it to settle (steady state) OR
   Perform calibration experiments and choose a fixed time delay for a single reading
- Read instantaneous current (shunt resistor) immediately after potential reading
- Use value of steady state current and inner electrode potential to back calculate resistance.
- Use probe factor (calibration) to determine resistivity/conductivity of fluid.



#### Method #1: Wenner (steady state)

#### Pros

- Programmatically simple to implement
- Larger sample sets can be taken at steady state to reduce the effects of noise
- Provides quantitative conductivity data

#### Cons

- Relatively large amount of energy required per measurement
- Can produce significant ionic concentration gradients over time in stagnant solutions (drift)



#### Method #2: Current interrupt (instant off)

Use Wenner method, but with the following modifications:

- Interrupt current by driving the digital out to low/zero (add a pull down resistor) OR Using a transistor to switch current source off
- Quickly record inner electrode potential after interrupt to determine the instant change (step).
- Use value of current just before interrupt and instant potential step magnitude (Ohmic) to back out an effective resistance.





#### Method #2: Current interrupt (instant off)

#### Pros

- Provides quantitative conductivity data
- Greater accuracy and repeatability than single point Wenner measurement

#### Cons

- Potentially time / energy intensive waiting for voltage to settle
- Programmatically more difficult to implement
- Relatively sensitive to noise and microcontroller timing delays



#### Method #3: AC Impedance

- Apply a high-frequency (100-500kHz), low amplitude (5mV) AC potential waveform between 2 electrodes.
- Measure the amplitude of the resulting current signal (shunt)
- Calculate the impedance (resistance)
- Can use third electrode as pseudoreference to improve accuracy or multiplex to test for electrode fouling



#### Method #3: AC Impedance

#### Pros

- Provides quantitative conductivity data
- Fast measurement, requires minimal energy\*\*
- Do not need to separate Ohmic and polarization components

#### Cons

- Additional electronic components required
- Sensitive to noise (for low-amplitude signal)

\*\*additional electronics may significantly increase power

#### Method #4: Dissimilar metal comparison

- Build sensing element with dissimilar metals ٠ having a significant difference in corrosion potentials (e.g. nickel and aluminum)
- Measure the potential between the electrodes.
- If liquid is non-conductive, voltage will float, or, ٠ be zero if a large pull-down resistor is wired in parallel.
- If liquid is conductive, a positive voltage will develop
- 4 electrode probe can be multiplexed (E1 to E3, E2 to E3, E1 to E4, E3 to E4) to detect electrode fouling.





#### Method #4: Dissimilar metal comparison

#### Pros

- Passive measurement. Very low energy consumption.
- Rapid measurement (ms)
- Programmatically trivial to implement

#### Cons

- Qualitative (threshold) or semi-quantitative with calibration
- Sensitive to noise



#### **Test Results** Arduino Uno w/ fixed resistors

Actual Resistance (Ω)	Current (mA)	ΔV (mV)	Experimental Resistance (Ω)	Absolute Error (%)
47	0.105	1	9.51	79.77
100	0.105	7	66.60	33.40
180	0.105	15	142.72	20.71
330	0.105	31	294.96	10.62
680	0.105	67	637.45	6.26
1500	0.105	156	1484.30	1.05
3000	0.105	317	3016.18	0.54
4700	0.105	490	4662.23	0.80
6800	0.105	725	6898.19	1.44
7500	0.105	791	7526.17	0.35
8200	0.105	873	8306.37	1.30
10000	0.105	1059	10076.11	0.76
15000	0.079	1183	15009.00	0.06

Large errors at low resistance values due to resolution limits of A/D converter (10bit). Very small voltage over inner electrodes.

Op amp unable to supply target current at high resistance value.



Functional prototype of sensing element

#### Graphite electrodes (3 mm) @ 5 mm OC

Epoxy mount





## Test Results

Arduino Uno stock solutions

Actual Conductivity (μS/cm)	Measured Conductivity (µS/cm)	Absolute Error (%)
186	185	0.54
686	629	8.26
1183	1151	2.70
2328	2961	27.21
5080	6296	23.93
7910	7391	6.56
10990	14813	34.79
41000	14483	64.68

Reference Conductivities:		
Seawater: 50,000 $\frac{\mu S}{cm}$		
Fresh water: $50 - 1500 \frac{\mu S}{cm}$		
Distilled water: $0.5 - 5 \frac{\mu S}{cm}$		

Gain can be set to provide better accuracy for high conductivity solutions, but requires additional noise reduction (filtering) and decreases the lower LoD.



#### **Dissimilar metal probe**

Functional prototypes created using:

1. Copper – aluminum electrodes in epoxy (500 - 600 mV)

2. Carbon steel - nickel electrodes in epoxy (300 - 400 mV)

• Same dimensions as graphite-epoxy probe



#### Thermoelectric generator (Peltier junction)

 Utilize temperature gradient between warm, insulated pipe and ambient air



6

8

4







# III: Energy harvesting element design and analysis Thermoelectric generator (Peltier junction)

• Need voltage boost converter to charge super capacitor



Peltier units tested: Thermonamic TEC1-12706 and Marlow TG16-6 82078

Boost converters tested: Maxim MAX630 and the Texas Instruments TL499A



Peltier resistive load benchtop testing ( $\Delta T \approx 40^{\circ}C$ )

#### TEC1-12706

Load Resistance	Test 1 (V <sub>g</sub> )
10Ω	1.058 V
100Ω	1.065 V
1kΩ	0.8126 V
10kΩ	0.7221 V
100k $\Omega$	0.7171 V

TG12-6 82078

Load Resistance	Test 1 (V <sub>g</sub> )
10Ω	1.067 V
100Ω	1.117 V
1kΩ	1.56 V
10kΩ	1.325 V
100kΩ	1.265 V

Short duration tests (<15 seconds) per point



Two TG12-6 82078 units in series

Load Resistance	Test 1 (V <sub>g</sub> )
10Ω	1.10 V
100Ω	2.07 V
1kΩ	2.32 V
10kΩ	2 <b>.</b> 75 V
100kΩ	2.49 V



Boost regulator testing w/ power supply input

## **MAX630**

 $V_{in} = 2.3 V$ 0.5F super capacitor load

Not viable due to excessive charge times and high minimum input voltage

Charge/Discharge	MAXIM (V <sub>in</sub> = 2.3V) 0.5F cap
Dt 0.0V - > 2.0V	20:01.7 (min:sec)
Dt 2.0V - > 3.0V	28:56.5
Dt 3.0V - > 4.0V	13:46.8
Dt 4.0V - > 5.0V	16:51.4
Dt 5.0V - > 6.0V	19:40.2
Dt 6.0V - > 7.0V	24:34.7
Dt 7.0V - > 8.0V	36:19.2
Dt 8.0V - > 9.0V	50:52.0
Dt 9.0V - > 3.0V	00:57.7
Dt 3.0V - > 0.5V	02:16.1
Dt 0.5V -> 90mV	03:52.8
Dt 90mV -> 50mV	02:12.0
Dt 50mV -> 25mV	03:51.8



Boost regulator testing w/ power supply input

ΤΙ 400		
	Charge/Discharge	TL499 (Vin = 1.5V), 0.5F cap
$V_{in} = 1.5 V$	Dt 0.0V - > 9.0V	100.68s
0.5F super capacitor load	Dt 9.0V - > 4.5V	38.33s

Charge/discharge times are acceptable



Boost regulator w/ 2x series Peltier

# TL499 – 2X TG12-6 82078

 $\Delta T = 40^{\circ}C$  o.5F super capacitor load

Voltage (V <sub>o</sub> )	Time (H:M:S)
0.2317 V	0:00:00
0.442 V	1:02:52
0.442 V	Test was ended

- Stall in charging due to thermal saturation of Peltier junction
- Peltier junction unable to produce enough voltage/current to continue charge
- Cycling as boost regulator cut in and out (min voltage)



#### Takeaways:

- Large heat sinks and/or active cooling likely required for viable TEG energy harvesting from warm (140-200 °F) insulated pipes.
- Additional electronics and or larger footprint TEG's required for reasonable charge times.
- Serious concern from industry partners about large perforations in insulation
- Only viable for insulated, warm lines
- Solar charging a better option







- Designed to support conductivity measurement
- \$13 / board (node)
  (solar cell, enclosure not included)





Header pin connections to externally connected sensors, with controlled power, ground, three analog inputs and 3 digital input pins.







- Salt on sensor with lip (hold water)
- Rain triggers conductive readings
- Galvanic / binary sensor (steel Ni)





#### Time from last node update vs time of update

0:17:17 0 0:14:24 TIME FROM LAST UPDATE (MM:SS) Ø 0:11:31  $\bigcirc$ 0:08:38 0  $\odot$ 0 0:05:46 0:02:53 0:00:00 7:12:00 9:36:00 12:00:00 14:24:00 16:48:00 19:12:00 21:36:00 0:00:00 0:00:00 2:24:00 4:48:00 TIME OF NODE UPDATE RECIEVED (HH:MM:SS)

⊚Node 2



**Conductivity Test Node 8** 





#### **Performance:**

Direct sunlight: ~ 1 min/sample

**Diffuse sun / overcast:** 3-20 min/sample

#### Average current draw (@ 3.3V):

Measurement: 1-4 mA measurement Radio transmitting: 14 mA Listening mode: <1 mA

Average transmission rate: 20 – 300 ft/min (0.23 – 3.4 mph)



#### The good:

- Performance characteristics are reasonable for intended application
- Boards functioned reliably outside of user-error (bad solder joints)
- Galvanic sensor provided repeatable and discernable indication of electrolyte



#### The not-so-good:

- Noise from radio picked up by analog inputs <u>Solution</u>: low pass filter, separate grounded enclosure, shielded / twisted pair wiring
- Occasional errors from crowded radio frequencies <u>Solution</u>: better error checking than simple checksum
- Downtime / low sample rates during dark/overcast periods
  <u>Solution</u>: secondary RC transistor circuit (instead of cap burndown)



# Publications / presentations / theses / reports

R. Srinivasan, M. Cullin, T. Petersen, C. Forbes, "Testing of a Low-Power Wireless Sensor Network of Conductivity Probes to Detect of Corrosive Fluids in Pipelines (C2021-16380)," CORROSION 2021. April 18-22, 2021.

R. Srinivasan, M. Cullin, T. Petersen, C. Forbes, "Development of a Low-Power Wireless Sensor Network of Conductivity Probes to Detect Corrosive Fluids in Pipelines (C2020-14502)," CORROSION 2020. June 14-18, 2020. Cancelled (due to COVID-19). Reviewed, accepted, and published.

C. Forbes. "Development of a Low-powered Wireless Sensor Network of Conductivity Probes to Detect the Presence of Fluids That Cause Internal Pipeline Corrosion." M.S. thes., University of Alaska Anchorage, 2020.

C. Forbes, K. M., L. M., M. W., B. A., M. C.. "Conductivity Probe Design." Final report and presentation ME A438. Presented to / approved by Mechanical Engineering Department, 2019.

M. A., B. B., L. C., M. M., R. H. "Pressure Vessel Design." Final report and presentation ME A438. Presented to / approved by Mechanical Engineering Department, 2019.

T. Petersen, J.S. "Low Power Conductivity Sensor." Report for project-sponsored Summer UGRA, 2020.

T. Petersen, M. Cullin, K.T. "Wireless Sensor Network of Conductivity Probes." Report for project-sponsored Summer UGRA, 2021.



# Student Engagement

• engaged 12 undergraduate engineering students in design work related to the project

- supported 1 graduate student to develop the conductivity sensing element and measurement procedure
- supported three summer undergraduate research assistantships
- facilitated a program for practicing engineers from BP Alaska to mentor the undergraduate design teams associated with the project
- helped encourage one student to enter the pipeline industry (Hilcorp AK)





- Application to Corrosion Under Insulation, water ingress detection
- Explore certification to operate in potentially explosive atmospheres
- Application to oil conductivity (time-of-wetness) monitoring for buried pipelines
- Application to specialized cleaning pigs designed to separate oil and water
- Expanded energy harvesting techniques (vibration-based)

